

### 7) Coupling coefficient ( $k$ )

We will now establish an upper limit for the inductance  $M$ . The energy stored in the circuit cannot be negative because the circuit is passive. This means that the quantity  $(\frac{1}{2}L_1i_1^2 + \frac{1}{2}L_2i_2^2 - Mi_1i_2)$  must be greater than or equal to zero:

$$\frac{1}{2}L_1i_1^2 + \frac{1}{2}L_2i_2^2 - Mi_1i_2 \geq 0 \quad \dots(7.1)$$

To complete the square, we both add and subtract the term  $i_1i_2\sqrt{L_1L_2}$  on the right-hand side of Eq. (6.11) and obtain

$$\frac{1}{2}(i_1\sqrt{L_1} - i_2\sqrt{L_2})^2 + i_1i_2(\sqrt{L_1L_2} - M) \geq 0 \quad \dots(7.2)$$

The squared term is never negative; at its least it is zero. Therefore, the second term on the right-hand side of Eq. (6.12) must be greater than zero; that is,

$$\sqrt{L_1L_2} - M \geq 0$$

or

$$M \leq \sqrt{L_1L_2} \quad \dots(7.3)$$

Thus, the mutual inductance cannot be greater than the geometric mean of the self-inductances of the coils. The extent to which the mutual inductance  $M$  approaches the upper limit is specified by the *coefficient of coupling*  $k$ , given by

$$k = \frac{M}{\sqrt{L_1L_2}} \quad \dots(7.4)$$

$$M = k\sqrt{L_1L_2} \quad \dots(7.5)$$

Where  $0 \leq k \leq 1$  or equivalently  $0 \leq M \leq \sqrt{L_1L_2}$ .

The *coupling coefficient* is the fraction of the total flux emanating from one coil that links the other coil. For example, in Fig.6.2(a),

$$k = \frac{\phi_{12}}{\phi_1} = \frac{\phi_{12}}{\phi_{11} + \phi_{12}} \quad \dots(6.6)$$

and in Fig.6.2(b),

$$k = \frac{\phi_{21}}{\phi_2} = \frac{\phi_{21}}{\phi_{21} + \phi_{22}} \quad \dots(6.7)$$

- 1) For  $k = 1$  (the entire flux produced by one coil links another coil, 100% coupling) the coils are said to be *perfectly coupled*.
- 2) For  $k < 0.5$  coils are said to be *loosely coupled*;
- 3) For  $k > 0.5$ , coils are said to be *tightly coupled*.

The *coupling coefficient*  $k$  is a measure of the magnetic coupling between two coils;  $0 \leq k \leq 1$

*coupling coefficient*  $k$  depend on the closeness of the two coils, their core, their orientation, and their windings.

The air-core transformers used in radio frequency circuits are loosely coupled, whereas iron-core transformers used in power systems are tightly coupled. The linear transformers are mostly air-core; the ideal transformers are principally iron-core.

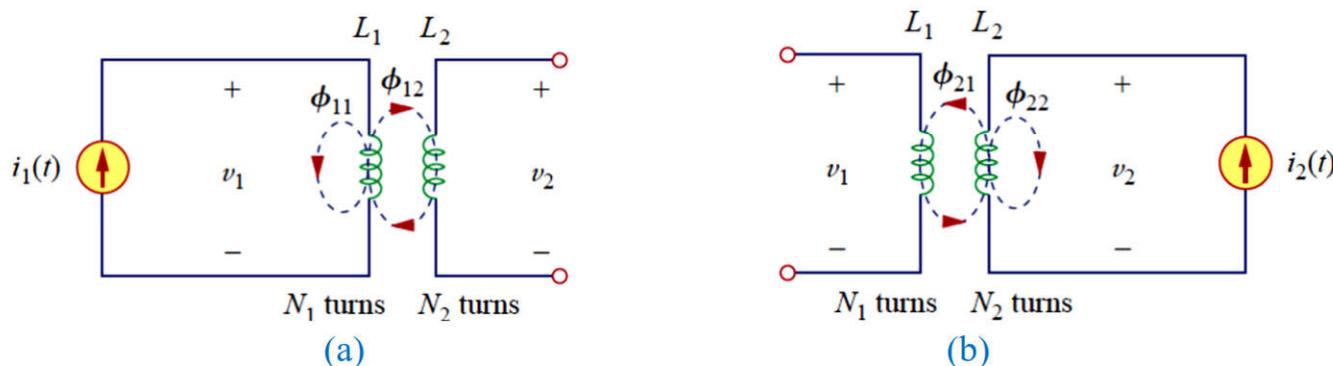


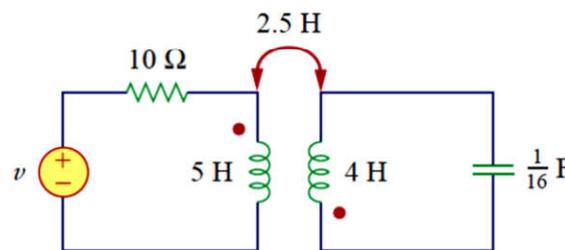
Fig.6.2

**Example 5:** Determine the coupling coefficient and calculate the energy stored in the coupled inductors at time  $t=1$  s if  $v = 60\cos(4t + 30^\circ)$  V.

**Solution:**

$$k = \frac{M}{\sqrt{L_1 L_2}} = \frac{2.5}{\sqrt{5 \times 4}} = 0.56 \quad (\text{tightly coupled})$$

To find the energy stored, we need to calculate the current. To find the current, we need to obtain the frequency-domain equivalent of the circuit.



$$\begin{aligned} 60 \cos(4t + 30^\circ) &\Rightarrow 60 \angle 30^\circ, \quad \omega = 4 \text{ rad/s} \\ 5 \text{ H} &\Rightarrow j\omega L_1 = j20 \Omega \\ 2.5 \text{ H} &\Rightarrow j\omega M = j10 \Omega \\ 4 \text{ H} &\Rightarrow j\omega L_2 = j16 \Omega \\ \frac{1}{16} \text{ F} &\Rightarrow \frac{1}{j\omega C} = -j4 \Omega \end{aligned}$$

The frequency-domain equivalent is shown in Fig.. Now apply mesh analysis.

For mesh 1,

$$(10 + j20)I_1 + j10I_2 = 60 \angle 30^\circ \quad \dots(1)$$

For mesh 2,

$$j10I_1 + (j16 - j4)I_2 = 0 \quad \dots(2)$$

Solve Eq.s (1) and (2) we get,

$$I_1 = 3.905 \angle -19.4^\circ \text{ A} \quad \& \quad I_2 = 3.254 \angle 160.6^\circ \text{ A}$$

In time domain.

$$i_1 = 3.905 \cos(4t - 19.4^\circ) \quad \& \quad i_2 = 3.254 \cos(4t + 160.6^\circ)$$

At  $t=1$ s,  $4t = 4 \text{ rad} = 229.2^\circ$

$$i_1 = 3.905 \cos(229.2^\circ - 19.4^\circ) = -3.389 \text{ A}$$